

AVEVA PI WORLD

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# Sustainable Process Design using AVEVA™ Process Simulation

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AVEVA

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# Agenda

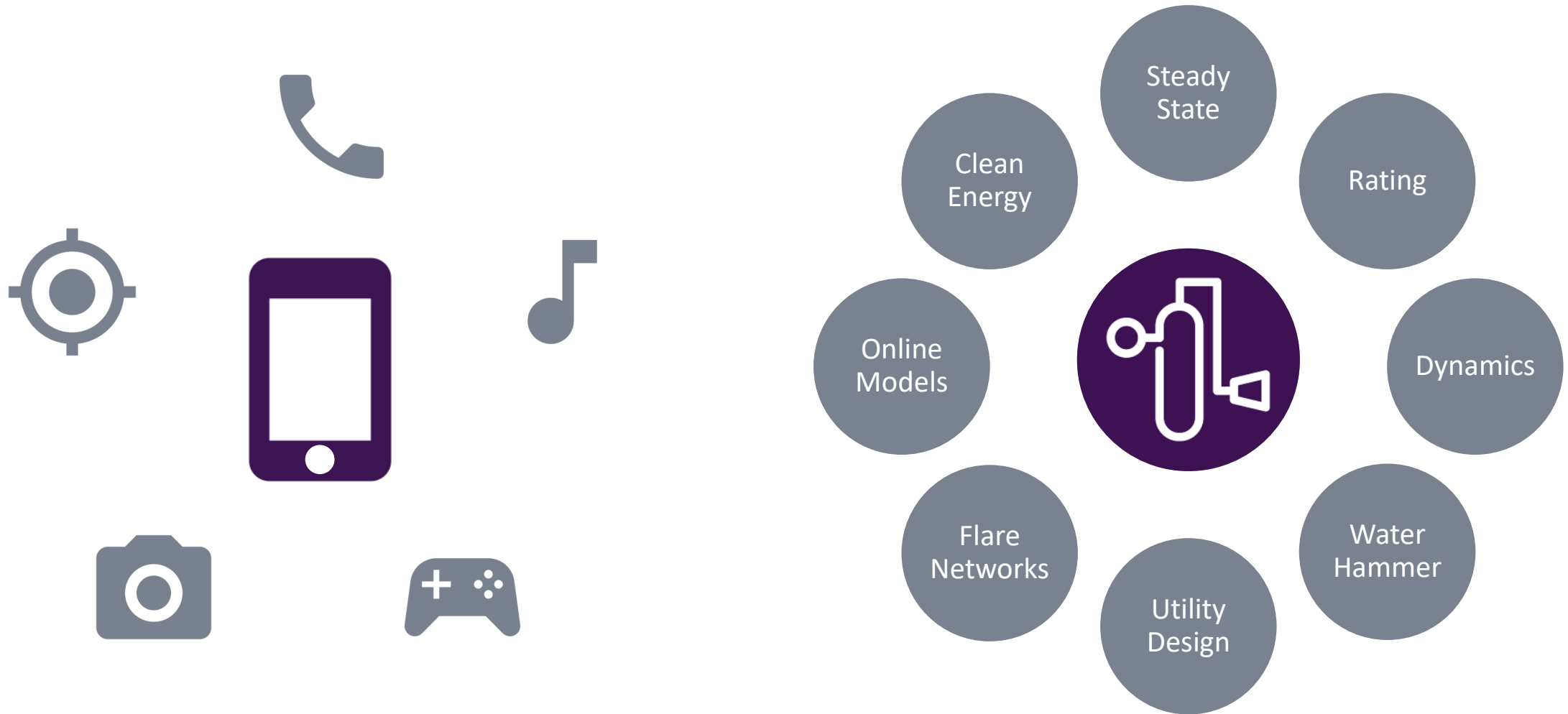
1. What is AVEVA Process Simulation?
2. Greenhouse Gas Emissions
3. Hydrogen Production
4. Renewable Energy
5. Takeaways

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# Introduction to AVEVA Process Simulation



# Reduce Total Ownership Cost and Engineering Hours



# AVEVA Process Simulation – Driving Digital Transformation

Designed from the ground up, delivering the process digital twin, to the next generation of engineers



**Designed from the Ground Up**

- Multi-core
- Continuously saved for cloud
- Role-based user interface
- Open model writing

**50% reduction in simulation effort across the lifecycle**

**Collaboration internally and externally**



**Delivering the Process Digital Twin**

- Design, Rating and Dynamic modes
- Libraries for different assets
- One single model for the entire asset lifecycle

**Adaptable for sustainable process development**

**Improved engineering workflow**



**To the Next Generation of Process Engineers**

- Groundbreaking ease of use
- Instantaneous results
- Intuitive user interface

**Enables true Digital Transformation**

# AVEVA Process Simulation Capabilities

## Ease of Use

The **continuously-solved** and **highly-interactive** behavior with **Undo** enables rapid problem exploration and fast adoption by next-generation users.

## SimSci Thermodynamics

Proven **SimSci** thermodynamics and data import based on industry standards provides high-speed and accurate solutions with all major **thermo methods**.

## Equation-Oriented Solver

A robust **equation-oriented solver** using state-of-the-art numerics allows for efficient calculation especially when there are lots of recycles.

## Steady-State & Dynamics

Seamless switching between **steady state**, **rating**, and **dynamic** modes drives collaboration across engineering domains and model reuse through the project lifecycle.

## Library Approach

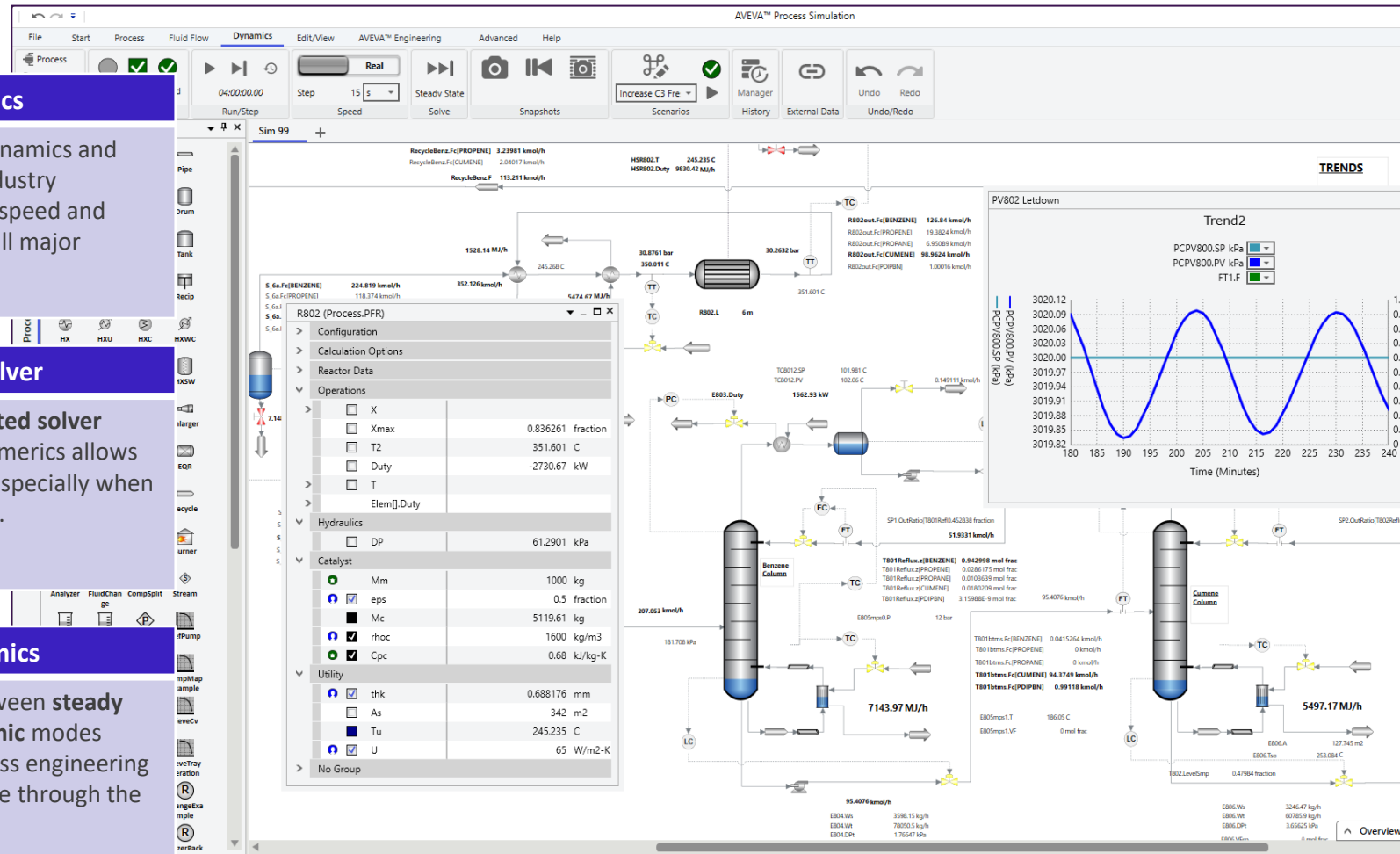
Model libraries for process utilities (**steam**, **cooling water**, **flares**), as well as **process simulation** allows a common platform for process department simulation.

## Open Modeling

Access to the **mathematical equations** enables process engineers to both customize and add new equipment models without programming.

## New Applications

The **open platform extendable** architecture allows the expansion of process simulation into other industries such as batch, power, and more

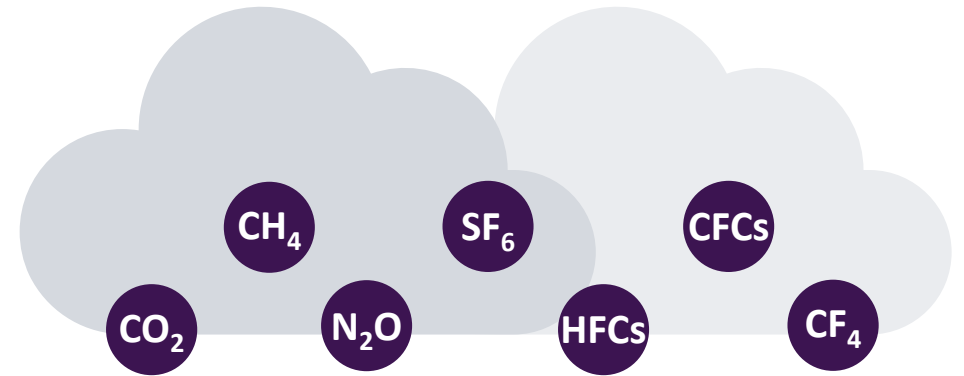


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# Greenhouse Gas (GHG) Emission Calculations

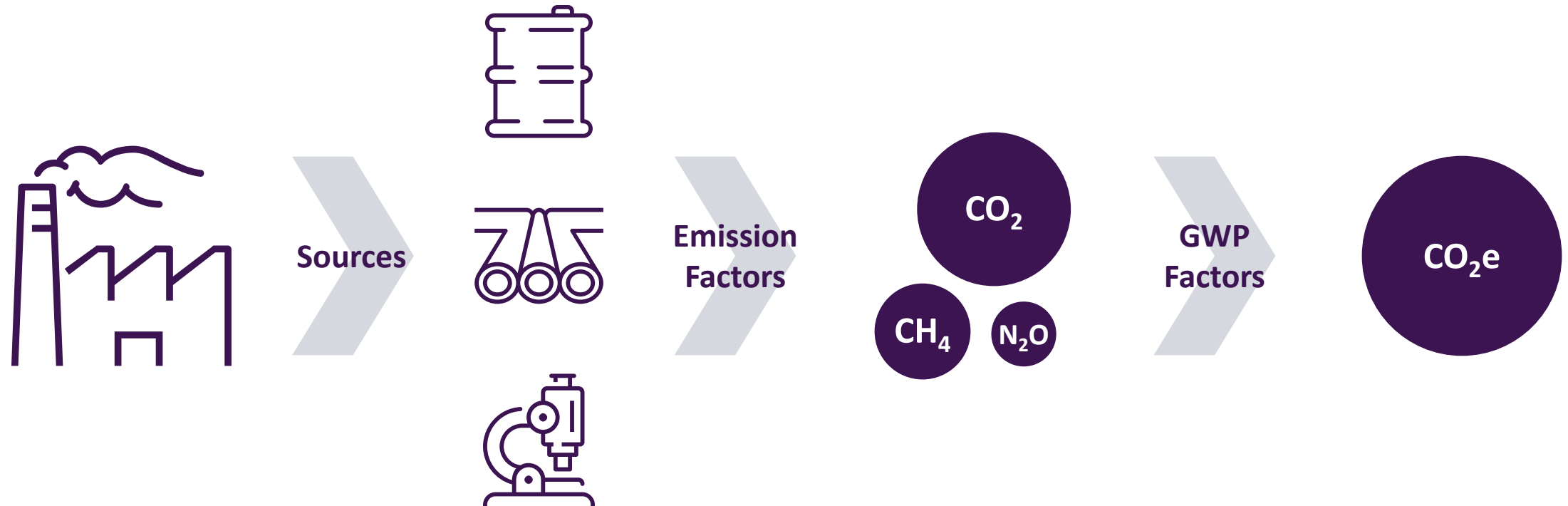
# Greenhouse Gas Emissions

- Nearly all processes release GHGs into the atmosphere through:
  - Stationary combustion
  - Combustion of waste gases
  - Purchased gases
  - Indirect emissions from purchased steam and electricity
- Most countries have begun to limit GHG emissions and have strict targets for reducing them
- AVEVA Process Simulation can calculate greenhouse gas emissions and optimize processes to reduce the overall carbon footprint
- GHG models are included in the **Economics** library of AVEVA Process Simulation

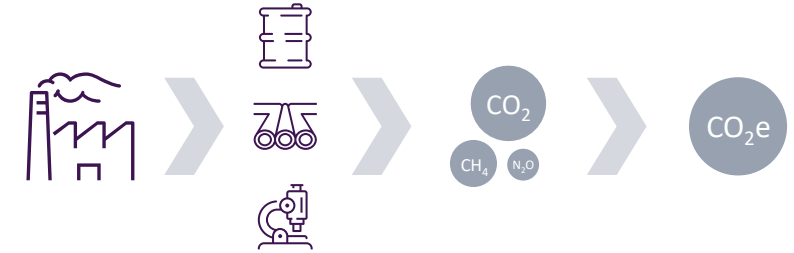




# How to Calculate GHG Emissions?



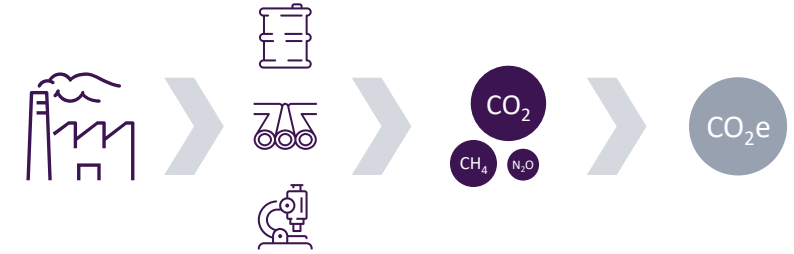
# Types of Emission Sources



- The US Environmental Protection Agency (EPA) separates emissions into 3 unique ‘scopes’
- Scope 1 – Direct emissions from your organization
  - **Stationary Combustion, Waste Gas, Purchased Gases**, Mobile Sources, Refrigeration, Fire Suppression
- Scope 2 – Indirect emissions from energy and steam generation
  - **Steam**, Electricity
- Scope 3 – Other indirect emissions from your value chain
  - Business Travel, Commuting, Product Transport, Waste

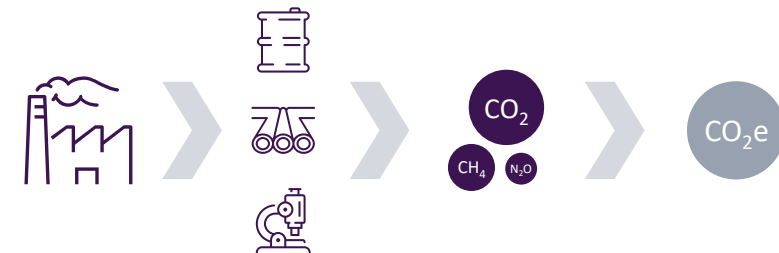
Calculated in AVEVA Process Simulation

# Understanding Emission Factors (EFs)



- Emission Factors describe the **quantity of pollutant** released from a material per **unit**
  - For example, stationary combustion of Natural Gas produces about 53.06 [kg CO<sub>2</sub> / MMBtu] = 0.0544 [kg CO<sub>2</sub> / scf]
- Common units are mass of pollutant per weight, volume, energy, or time
- EFs can be calculated for every material at various stages of the product lifecycle
  - What quantity of emissions are produced per kg of material produced?
  - What quantity are produced per kg of material burned?

# EFs in AVEVA Process Simulation

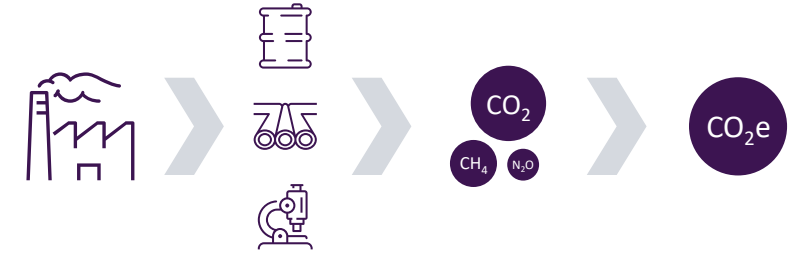


- AVEVA Process Simulation provides default emission factor submodels for common fuels:
  - Natural Gas (**NatGasEF**)
  - No. 2 Fuel Oil (**No2FuelEF**)
  - No. 6 Fuel Oil (**No6FuelEF**)
- You can use the **DefEF** submodel as a template for defining emission factors for other materials
- AVEVA Process Simulation requires a mass per energy basis for EFs. Conversion from other units can be done within the custom submodel.



No2FuelEF (Economics.No2FuelEF)		
No Group		
<input type="checkbox"/>	EF_CO2	73.9852 kg/MMBtu
<input type="checkbox"/>	EF_CH4	2.971 g/MMBtu
<input type="checkbox"/>	EF_N2O	0.579708 g/MMBtu
<input checked="" type="checkbox"/>	HHV	1.03231E+6 Btu/ft3
<input checked="" type="checkbox"/>	EFv_CO2	76.3761 kg/scf
<input checked="" type="checkbox"/>	EFv_CH4	3.06701 g/scf
<input checked="" type="checkbox"/>	EFv_N2O	0.598442 g/scf

# What is Global Warming Potential (GWP)?

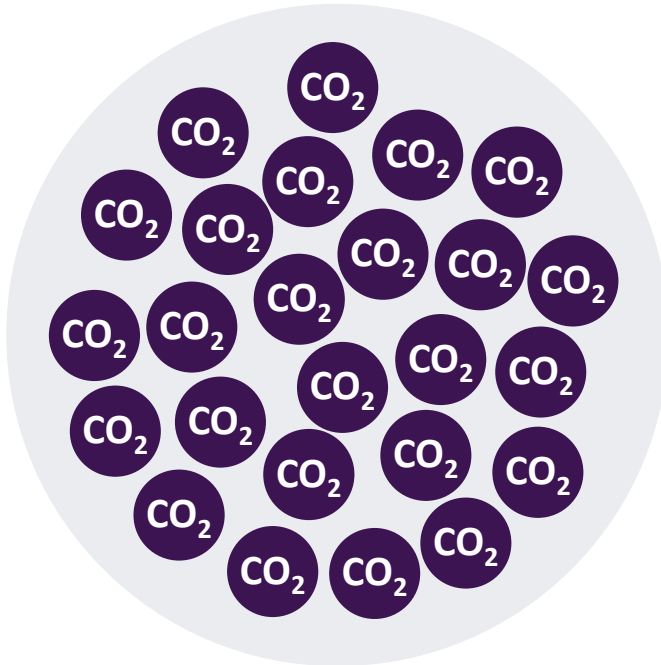


- Not all GHG emissions have the same warming potential
- Global Warming Potential (GWP) factors are used to align emissions to a common scale
- $\text{GWP} = \text{energy absorbed by 1 ton of Gas A} / \text{energy absorbed by 1 ton of CO}_2$  (typically over 100 years)
- Measured experimentally while accounting for:
  - Radiative Efficiency – how much energy does the GHG absorb?
  - Lifetime – how long will the GHG remain in the atmosphere before being broken down?

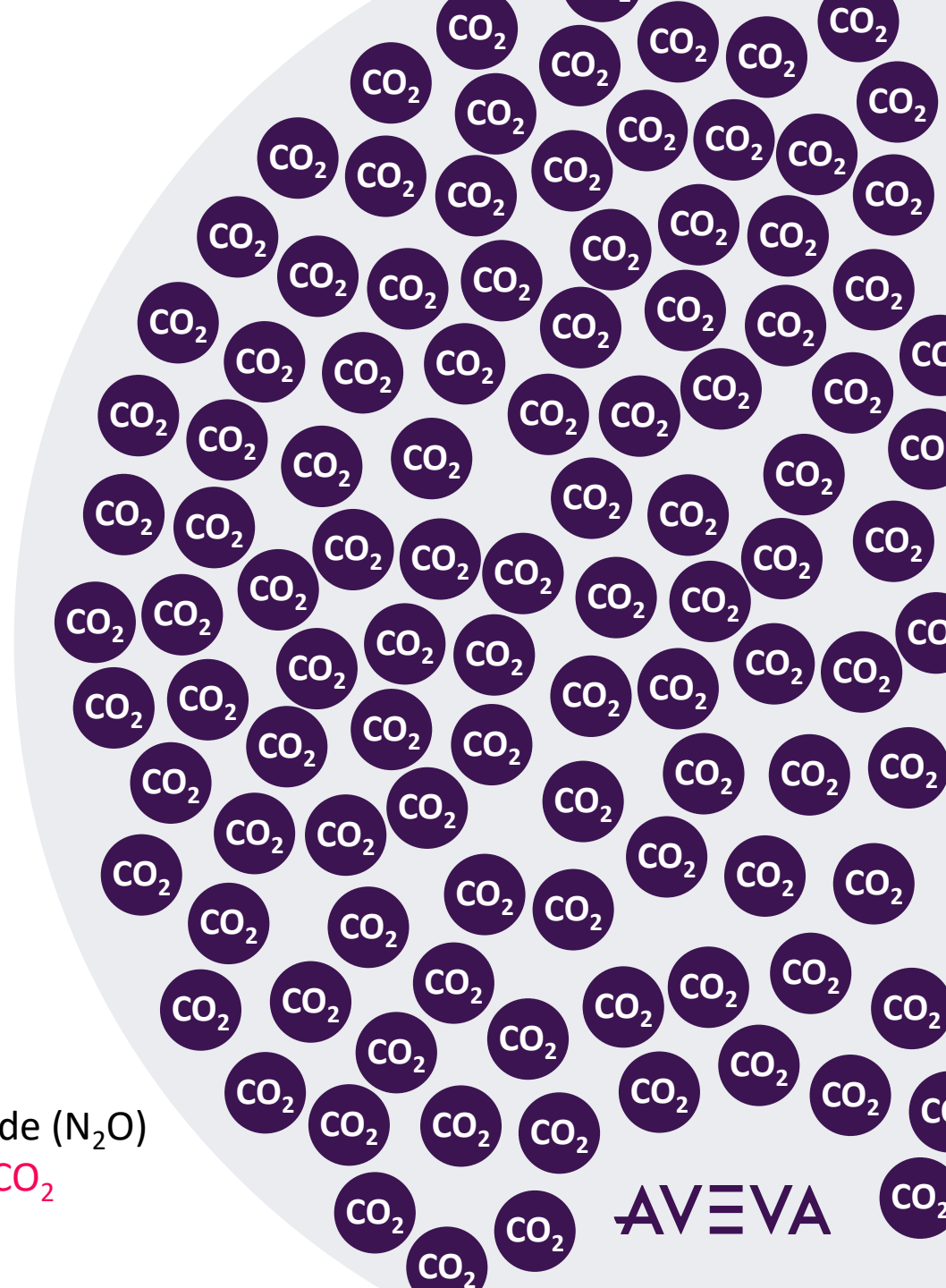
# Visualizing Global Warming Potential



Carbon Dioxide (CO<sub>2</sub>)  
1x CO<sub>2</sub>



Methane (CH<sub>4</sub>)  
25x CO<sub>2</sub>

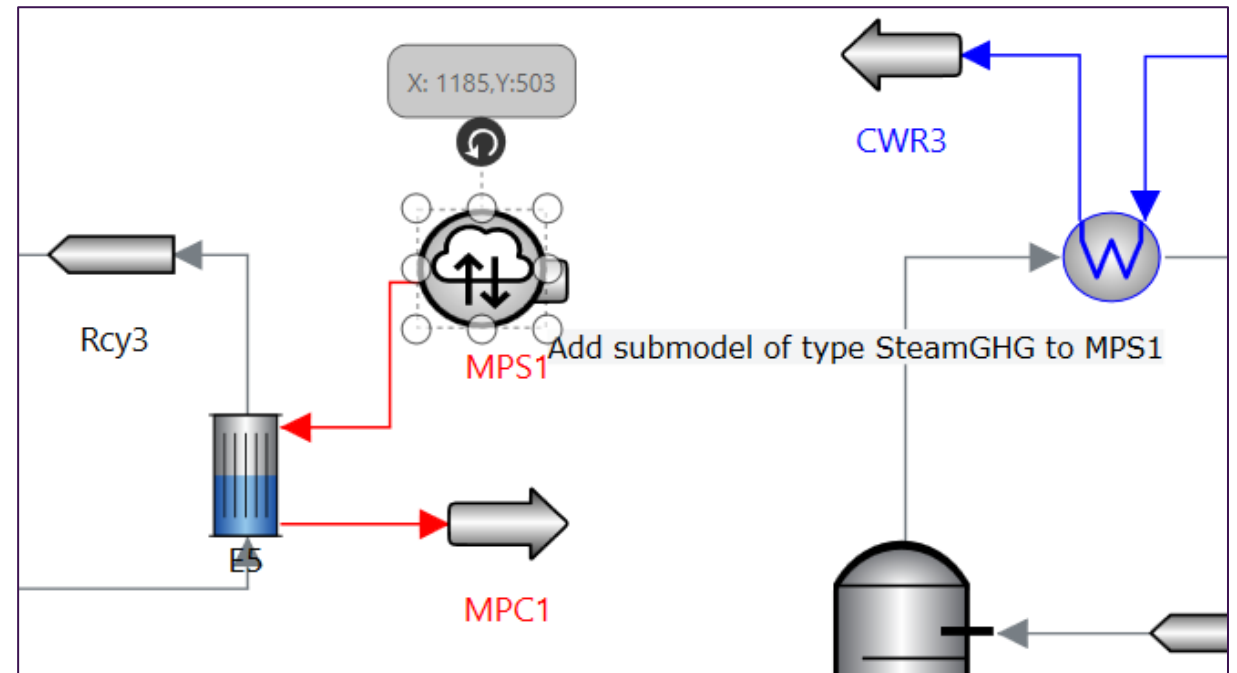


Nitrous Oxide (N<sub>2</sub>O)  
298x CO<sub>2</sub>

# Calculating GHG Emissions in AVEVA Process Simulation

## Introduction

- AVEVA Process Simulation calculates the CO<sub>2</sub>-equivalent emissions (CO<sub>2</sub>e) across the entire simulation
- Drag + Drop GHG submodels on top of existing models in the simulation
- Access the full features of AVEVA Process Simulation
  - Optimization
  - Dynamic studies
  - Steady-state design



# Calculating GHG Emissions in AVEVA Process Simulation

## SummaryGHG Model

- Provides a single location to view total CO2e emissions
- Automatically sums emissions from all GHG submodels in the simulation

View and Edit GWP Factors

Total CO2e emissions for all emission sources

CO2e emissions for each source in Scope 1

Total Scope 1 CO2e emissions

CO2e emissions for each source in Scope 2

Total Scope 2 CO2e emissions

SummaryGHG (Economics.SummaryGHG)		
Global Warming Potential (GWP) Factors		
<input checked="" type="checkbox"/>	GWP_CH4	25
<input checked="" type="checkbox"/>	GWP_N2O	298
Summary		
<input type="checkbox"/>	TotalCO2e	1.65645 t/h
Scope 1 Emissions		
<input type="checkbox"/>	TotalCombustGHG	0.300768 t/h
<input type="checkbox"/>	TotalWasteGHG	0.240079 t/h
<input type="checkbox"/>	TotalPurchasedGHG	0.708039 t/h
<input type="checkbox"/>	TotalCO2e_S1	1.24889 t/h
Scope 2 Emissions		
<input type="checkbox"/>	TotalSteamGHG	0.407566 t/h
<input type="checkbox"/>	TotalCO2e_S2	0.407566 t/h



# Calculating GHG Emissions in AVEVA Process Simulation

## CombustGHG Submodel

- Calculate emissions for stationary combustion (for example: burners, boilers, and furnaces)
- Emission Factors must be defined for the fuel:
  - Select a submodel (**Fuel**) that provides the correct emission factors *or*
  - Use the DefEF submodel and manually specify **EF\_CO2**, **EF\_CH4**, and **EF\_N2O**
- **CO2e** is calculated from individual CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O emissions with GWP factors defined in SummaryGHG model

GHG Emission Data		
	GHG.Fuel	Economics.No2FuelEF ▾
	GHG.EF_CO2	73.9852 kg/MMBtu
	GHG.EF_CH4	2.971 g/MMBtu ▾
	GHG.EF_N2O	0.579708 g/MMBtu ▾
	GHG.CO2e	67.792 kg/h ▾

Emission Factors for No. 2 Fuel Oil

GHG Emission Data		
	GHG.Fuel	Economics.DefEF ▾
		GHG.EF_CO2 75.04 kg/MMBtu
		GHG.EF_CH4 3 g/MMBtu
		GHG.EF_N2O 0.6 g/MMBtu
	GHG.CO2e	68.7615 kg/h ▾

Emission Factors Specified with DefEF

# Calculating GHG Emissions in AVEVA Process Simulation

## SteamGHG Submodel

- Calculate emissions for purchased steam
- Supports both calculation methods set by the US EPA
  - Set **CalcMethod** = **Supplier Factors** to manually specify emission factors from the steam supplier (*preferred*)
  - Set **CalcMethod** = **Boiler Efficiency** if supplier factors are unknown. Then, select a fuel and specify a boiler efficiency (**eta**).
- **CO2e** is calculated from individual CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O emissions with GWP factors defined in SummaryGHG model

GHG Emission Data		
<input type="radio"/>	GHG.CalcMethod	Supplier Factors ▾
<input type="radio"/>	GHG.Factors	Economics.DefEF ▾
<input checked="" type="checkbox"/>	GHG.EF_CO2	60 kg/MMBtu ▾
<input checked="" type="checkbox"/>	GHG.EF_CH4	2.8 g/MMBtu ▾
<input checked="" type="checkbox"/>	GHG.EF_N2O	0.25 g/MMBtu ▾
<input type="checkbox"/>	GHG.CO2e	54.9265 kg/h

Supplier Factor Method

GHG Emission Data		
<input type="radio"/>	GHG.CalcMethod	Boiler Efficiency ▾
<input type="radio"/>	GHG.Factors	Economics.NatGasEF ▾
<input checked="" type="checkbox"/>	GHG.eta	0.82 fraction
<input type="checkbox"/>	GHG.EF_CO2	53.0602 kg/MMBtu ▾
<input type="checkbox"/>	GHG.EF_CH4	1.00389 g/MMBtu ▾
<input type="checkbox"/>	GHG.EF_N2O	0.0974655 g/MMBtu ▾
<input type="checkbox"/>	GHG.CO2e	73.9425 kg/h ▾

Boiler Efficiency Method

# Calculating GHG Emissions in AVEVA Process Simulation

## WasteGHG Submodel

- Calculate emissions for waste gas combustion (for example: flaring, thermal oxidizers)
- To automatically calculate carbon content of waste stream, set **CalcMethod = Automatic**
- To manually map your fluid components to a standard waste composition, set **CalcMethod = Map Components**
  - Recommended for fluids where exact chemical formulas are not known for every component
  - You must provide a mapping submodel (see **DefMapWG**)
- CO<sub>2</sub>e emissions are calculated from flow rate, carbon content, and **Oxidation** fraction

GHG Emission Data		
<input checked="" type="checkbox"/>	GHG.CalcMethod	Automatic ▾
<input checked="" type="checkbox"/>	GHG.WasteCompMap	Economics.DefMapWG ▾
<input checked="" type="checkbox"/>	GHG.Oxidation	0.98 fraction
<input type="checkbox"/>	GHG.CO2e	317.942 kg/h ▾

Automatically Calculate Carbon Content

# Calculating GHG Emissions in AVEVA Process Simulation

## Purchased GHG Submodel

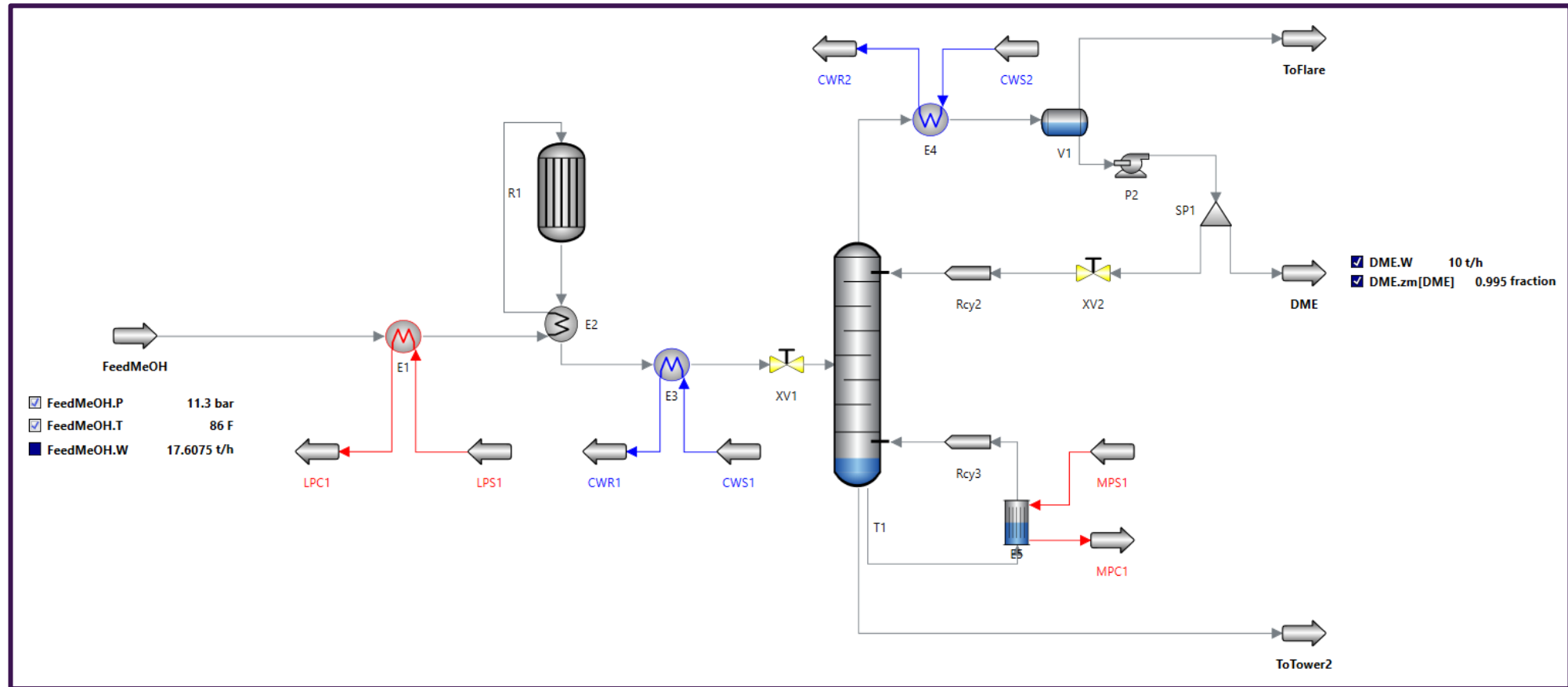
- Calculate emissions for purchased industrial gases (for example: refrigerants, laboratory gases)
- Specify the GWP factor for the purchased gas
  - Not sure? Visit the US EPA Center for Corporate Climate Leadership's [GHG Emission Factors Hub](#)

GHG Emission Data			
<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	GHG.GWP	14800
<input type="checkbox"/>	<input type="checkbox"/>	GHG.CO2e	157.1 kg/h

CO2e emissions for HFC-23

# Calculating GHG Emissions in AVEVA Process Simulation

## Full Example with Optimization



# Calculating GHG Emissions in AVEVA Process Simulation

## Step 1: Add SummaryGHG Model to Simulation and Confirm GWP Factors

SummaryGHG (Economics.SummaryGHG)			
Global Warming Potential (GWP) Factors			
<input checked="" type="checkbox"/>	GWP_CH4	25	
<input checked="" type="checkbox"/>	GWP_N2O	298	
Summary			
<input type="checkbox"/>	TotalCO2e	0 t/h	
Scope 1 Emissions			
<input type="checkbox"/>	TotalCombustGHG	0 t/h	
<input type="checkbox"/>	TotalWasteGHG	0 t/h	
<input type="checkbox"/>	TotalPurchasedGHG	0 t/h	
<input type="checkbox"/>	TotalCO2e_S1	0 t/h	
Scope 2 Emissions			
<input type="checkbox"/>	TotalSteamGHG	0 t/h	
<input type="checkbox"/>	TotalCO2e_S2	0 t/h	

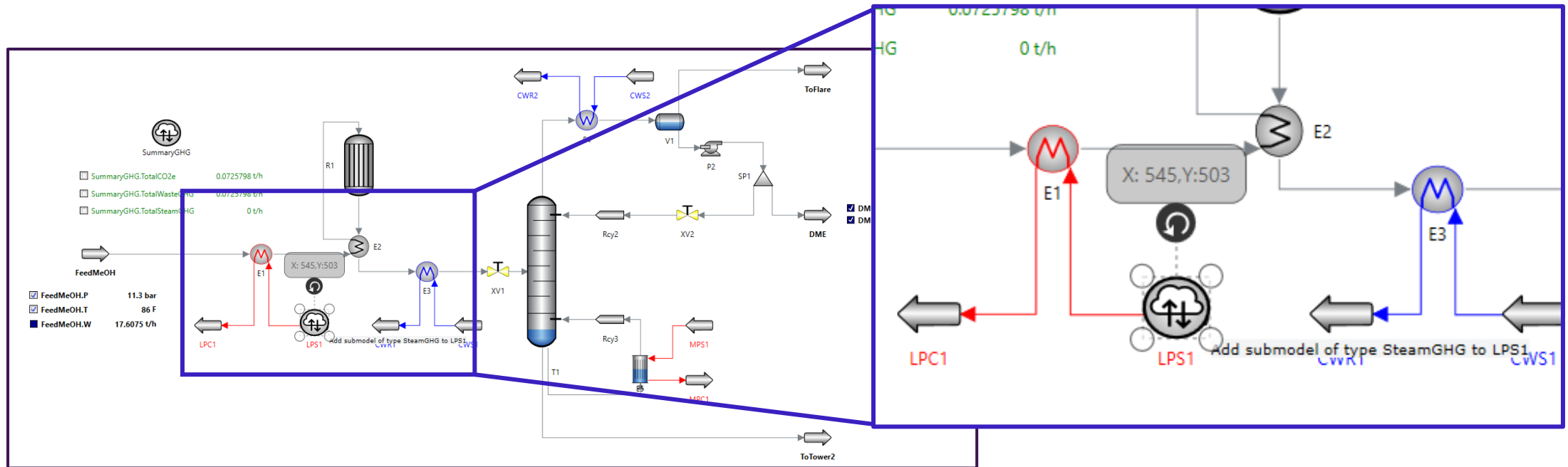


SummaryGHG

<input type="checkbox"/>	SummaryGHG.TotalCO2e	0 t/h
<input type="checkbox"/>	SummaryGHG.TotalWasteGHG	0 t/h
<input type="checkbox"/>	SummaryGHG.TotalSteamGHG	0 t/h

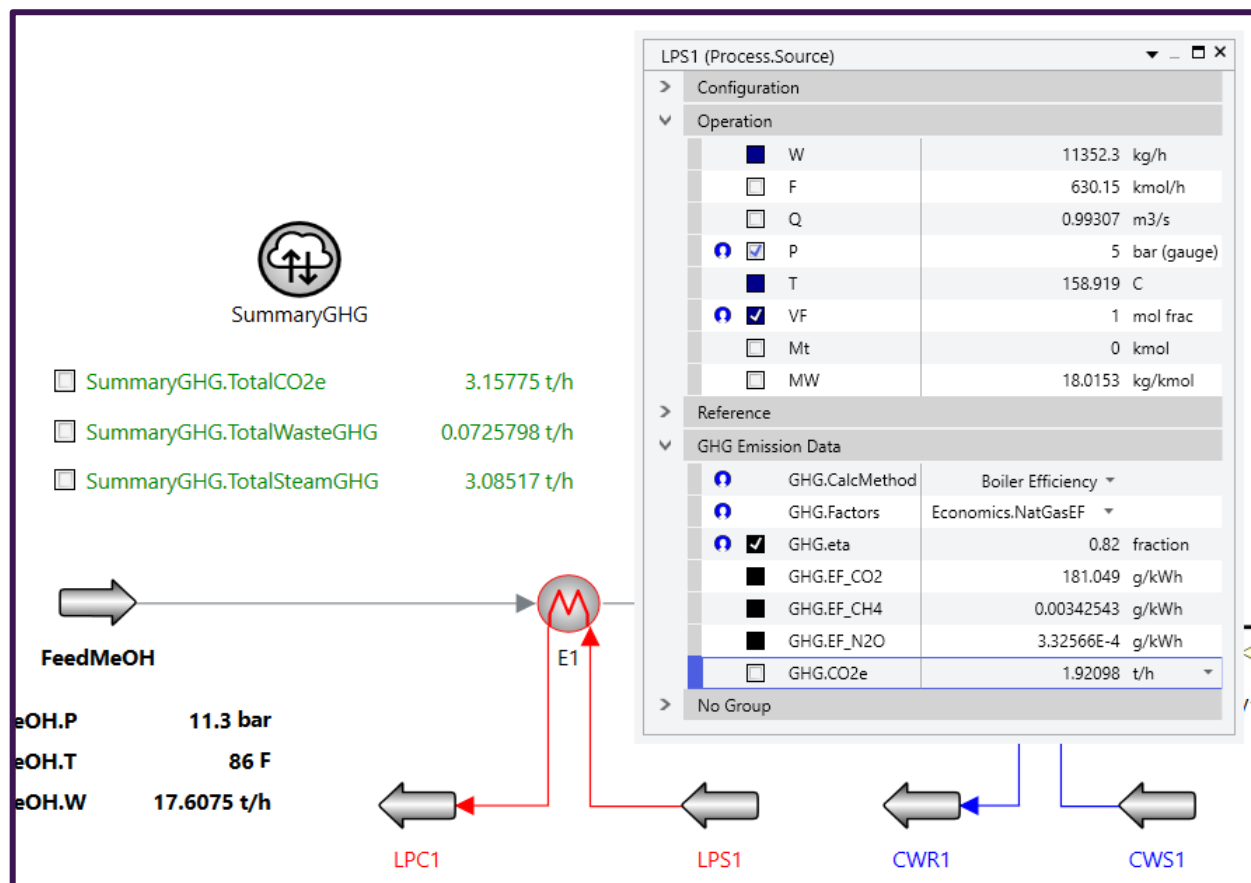
# Calculating GHG Emissions in AVEVA Process Simulation

## Step 2: Drag-and-Drop GHG Submodels into Steam Sources and Waste Gas Sinks



# Calculating GHG Emissions in AVEVA Process Simulation

## Step 3: Select Fuel Type and Set Efficiency in SteamGHG Submodels





# Calculating GHG Emissions in AVEVA Process Simulation

## Step 4: Create an Optimization Set

Optimization Set Editor

General

Name: Minimize GHG

Description: Minimize GHG emissions by adjusting column reboil ratio

Objective Function

☐ Maximize ☒ Minimize

SummaryGHG.TotalCO2e

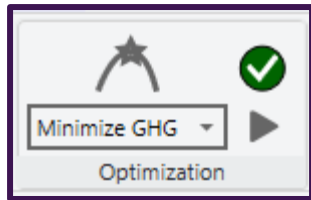
Variables


Status	Name	Value	Lower Bound	Upper Bound	Units
●	T1.ReboilRatio	4	0.2	10	

Run


# Calculating GHG Emissions in AVEVA Process Simulation

## Step 5: Run Optimization and Review Results



 SummaryGHG		
<input type="checkbox"/>	SummaryGHG.TotalCO2e	3.15775 t/h
<input type="checkbox"/>	SummaryGHG.TotalWasteGHG	0.0725798 t/h
<input type="checkbox"/>	SummaryGHG.TotalSteamGHG	3.08517 t/h

Before Optimization

 SummaryGHG		
<input type="checkbox"/>	SummaryGHG.TotalCO2e	2.10734 t/h
<input type="checkbox"/>	SummaryGHG.TotalWasteGHG	0.0628842 t/h
<input type="checkbox"/>	SummaryGHG.TotalSteamGHG	2.04446 t/h

After Optimization



# Hydrogen Production

# Hydrogen Production – Grey, Blue, or Green?

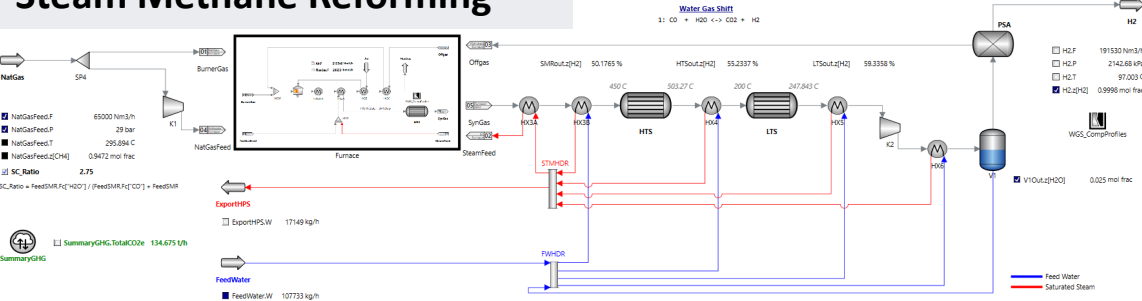
- Steam Methane Reforming (SMR) with Water Gas Shift (WGS) reactions
- CO<sub>2</sub> is a byproduct of both SMR and WGS reactions
- High reaction temperatures require large industrial furnaces
- **No carbon capture or storage**

- Steam Methane Reforming (SMR) with Water Gas Shift (WGS) reactions
- Carbon is **captured and stored** underground (CCS)
- However, not all carbon can be captured with current technologies

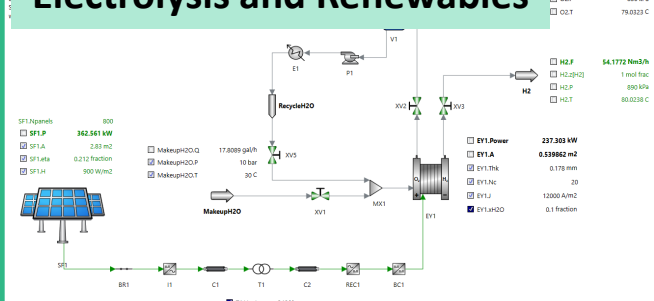
- Renewable energy sources to power water electrolysis
- Water is split into H<sub>2</sub> and O<sub>2</sub> with **no carbon** byproducts
- Only accounts for a small portion of all current hydrogen production

# Hydrogen Processing in AVEVA Process Simulation

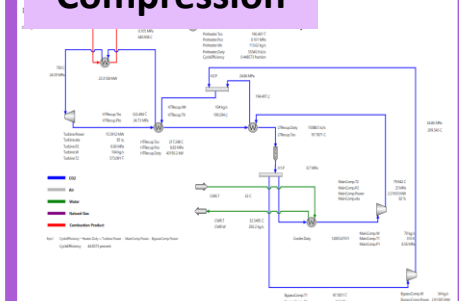
## Steam Methane Reforming



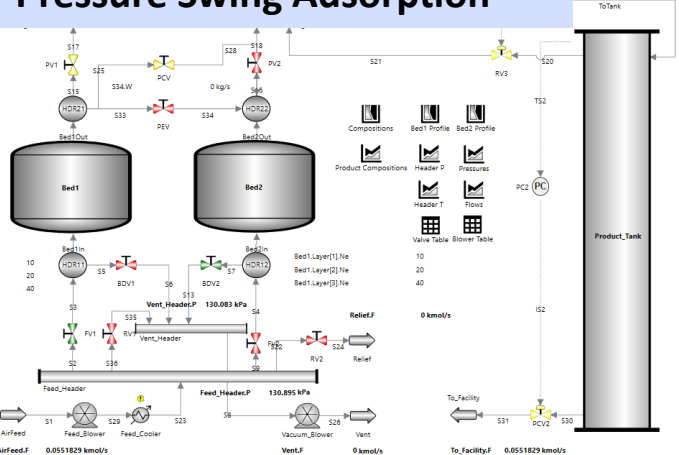
## Electrolysis and Renewables



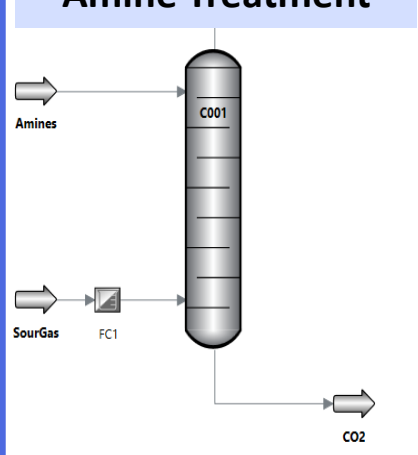
## Compression



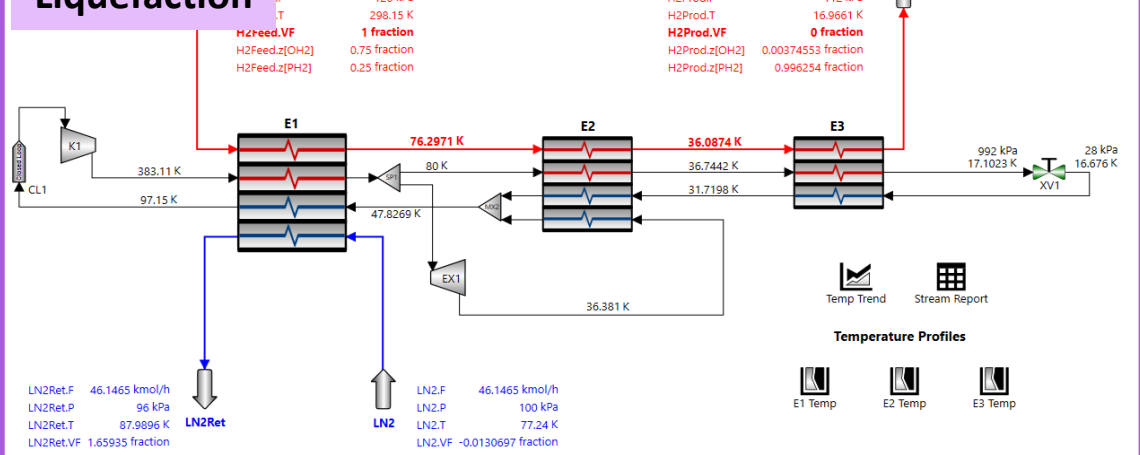
## Pressure Swing Adsorption



## Amine Treatment

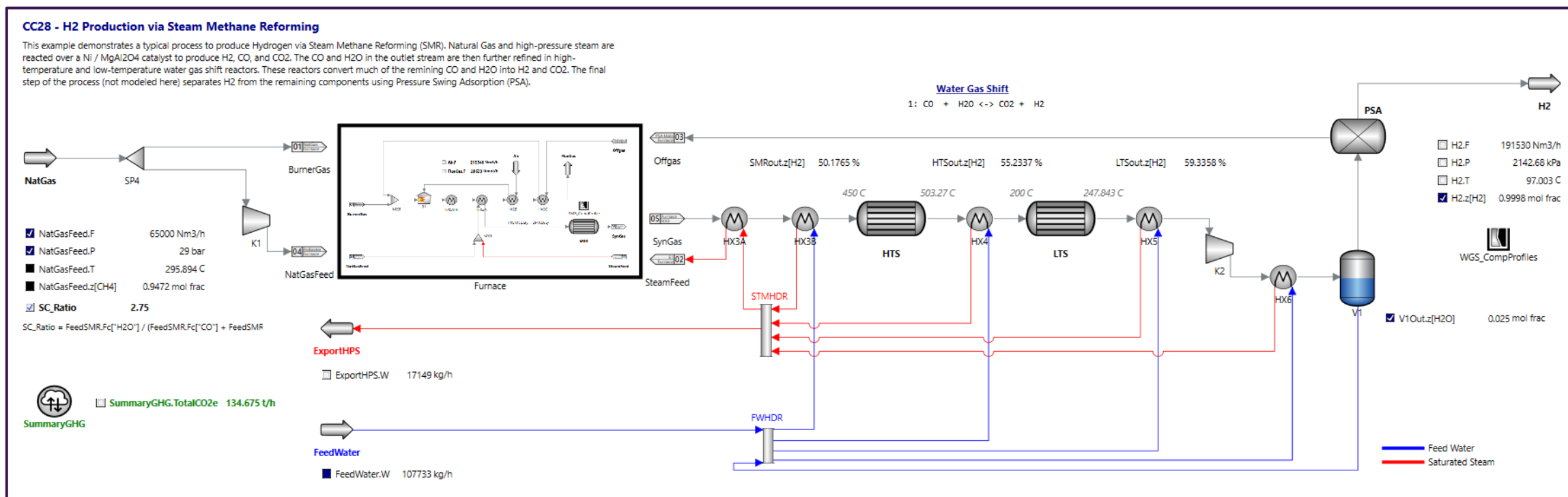


## Liquefaction

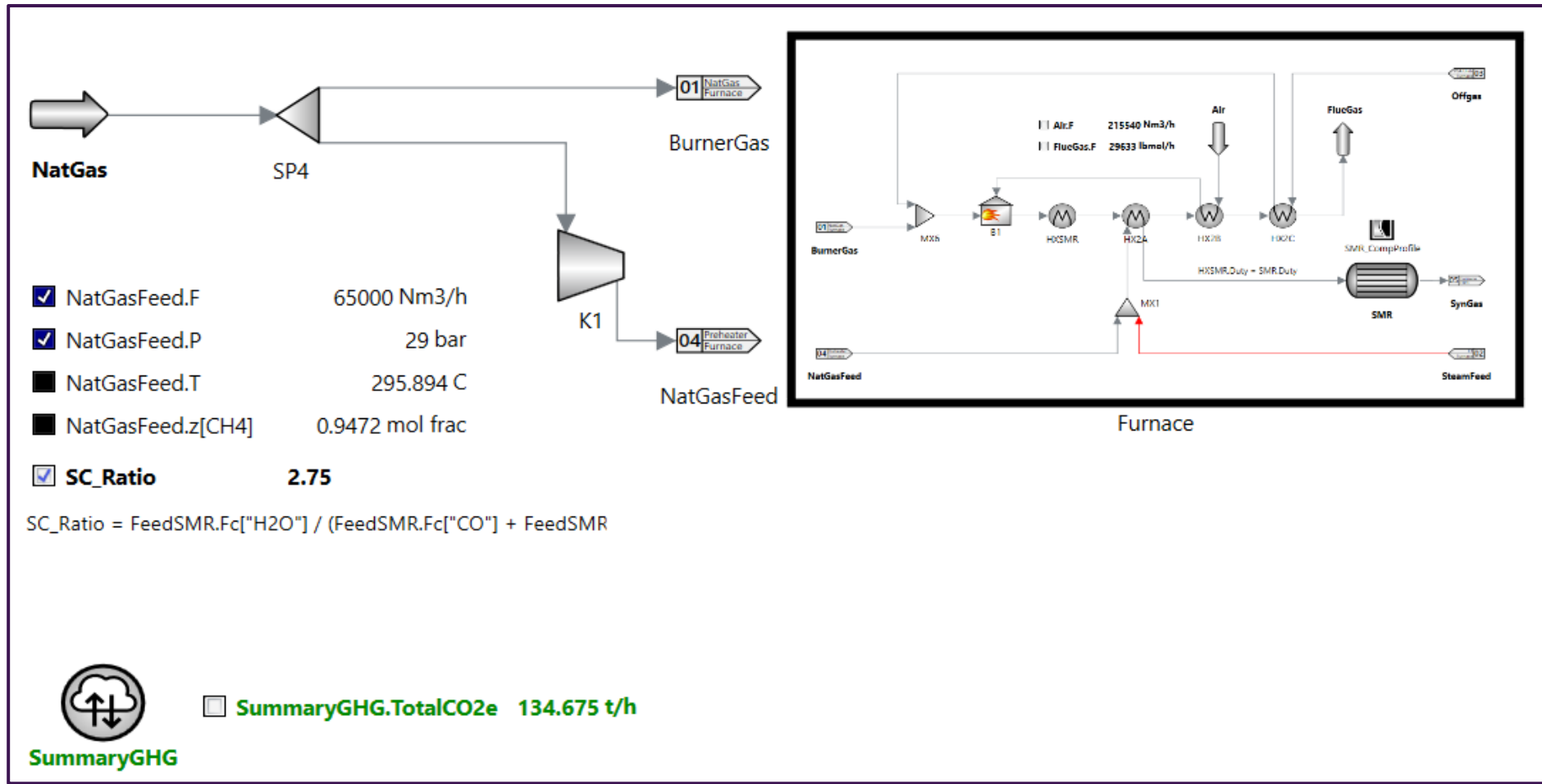


# Grey Hydrogen – SMR in AVEVA Process Simulation

- See Documented Example CC28 – H2 Production via Steam Methane Reforming



# SMR – Design Specifications



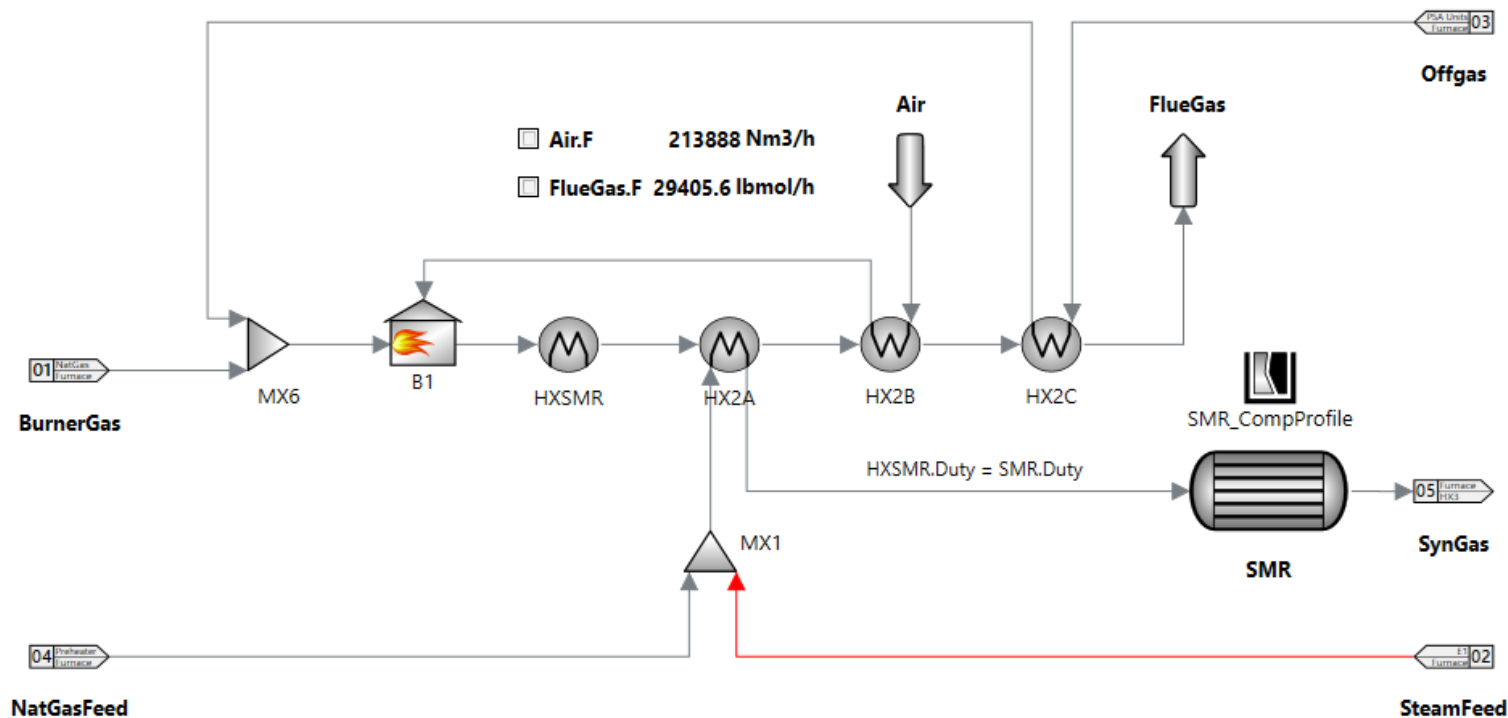
# SMR – Reformer Furnace

## Steam Methane Reforming

- 1:  $\text{CH}_4 + \text{H}_2\text{O} \leftrightarrow \text{CO} + 3\text{H}_2$
- 2:  $\text{CO} + \text{H}_2\text{O} \leftrightarrow \text{CO}_2 + \text{H}_2$
- 3:  $\text{CH}_4 + 2\text{H}_2\text{O} \leftrightarrow \text{CO}_2 + 4\text{H}_2$

☒ BurnerGas.F 810.673 Nm<sup>3</sup>/h  
☒ BurnerGas.P 200 kPa  
☒ BurnerGas.T 25 C

☒ NatGasFeed.F 65000 Nm<sup>3</sup>/h  
☒ NatGasFeed.P 2900 kPa  
☒ NatGasFeed.T 295.894 C  
☒ NatGasFeed.z[CH<sub>4</sub>] 94.72 mol%



☒ Offgas.F 93347.2 Nm<sup>3</sup>/h  
☒ Offgas.P 2142.68 kPa  
☒ Offgas.T 97.003 C  
☒ Offgas.z[CO<sub>2</sub>] 0.558658 mol frac

☒ Syngas.F 358585 Nm<sup>3</sup>/h  
☒ Syngas.P 1700.91 kPa  
☒ Syngas.T 850 C  
☒ Syngas.z[H<sub>2</sub>] 0.501765 mol frac

☒ SteamFeed.W 149829 kg/h  
☒ SteamFeed.P 2051.91 kPa  
☒ SteamFeed.T 840 C



# SMR – Reaction Kinetics

Equations			
Condition	Name	Status	Formula
	Eqn3	●	$\text{Rate}[\text{"H2O"}] = -\text{RateRxn}[1] - \text{RateRxn}[2] - 2 * \text{RateRxn}[3]$
	Eqn4	●	$\text{Rate}[\text{"H2"}] = 3 * \text{RateRxn}[1] + \text{RateRxn}[2] + 4 * \text{RateRxn}[3]$
	Eqn5	●	$\text{Rate}[\text{"CO"}] = \text{RateRxn}[1] - \text{RateRxn}[2]$
	Eqn25	●	$\text{Rate}[\text{not}[\text{"CO2"}, \text{"CH4"}, \text{"H2O"}, \text{"H2"}, \text{"CO"}]] = 0$
	Eqn6	●	$P_y = P / 100 * \text{tear}(z)$
	Eqn7	●	$k[1] = 4.225\text{E}15 * \exp(-240100 / (R * T))$
	Eqn8	●	$k[2] = 1.955\text{E}6 * \exp(-67130 / (R * T))$
	Eqn9	●	$k[3] = 1.020\text{E}15 * \exp(-243900 / (R * T))$
	Eqn10	●	$\text{Keq}[1] = \exp(-26830 / T + 30.114)$
	Eqn11	●	$\text{Keq}[2] = \exp(4400 / T - 4.036)$
	Eqn12	●	$\text{Keq}[3] = \text{Keq}[1] * \text{Keq}[2]$
	Eqn13	●	$\text{Ka}[\text{"CO"}] = 8.23\text{E}-5 * \exp(70650 / (R * T))$
	Eqn14	●	$\text{Ka}[\text{"H2"}] = 6.12\text{E}-9 * \exp(82900 / (R * T))$
	Eqn15	●	$\text{Ka}[\text{"CH4"}] = 6.65\text{E}-4 * \exp(38280 / (R * T))$
	Eqn16	●	$\text{Ka}[\text{"H2O"}] = 1.77\text{E}5 * \exp(-88680 / (R * T))$
	Eqn17	●	$\text{Ka}[\text{not}[\text{"CO"}, \text{"CH4"}, \text{"H2O"}, \text{"H2"}]] = 0$
	Eqn18	●	$\text{den} = 1 + \text{Ka}[\text{"CO"}] * \text{Py}[\text{"CO"}] + \text{Ka}[\text{"H2"}] * \text{Py}[\text{"H2"}] + \text{Ka}[\text{"CH4"}] * \text{Py}[\text{"CH4"}] + \text{Ka}[\text{"H2O"}] * \text{Py}[\text{"H2O"}] / \text{Py}[\text{"H2"}]$
	Eqn19	●	$\text{RateRxn}[1] * \text{den}^2 * 3600 = k[1] * \text{Py}[\text{"H2"}]^{(-2.5)} * (\text{Py}[\text{"CH4"}] * \text{Py}[\text{"H2O"}] - (\text{Py}[\text{"H2"}]^3 * \text{Py}[\text{"CO"}]) / \text{Keq}[1])$
	Eqn20	●	$\text{RateRxn}[2] * \text{den}^2 * 3600 = k[2] * \text{Py}[\text{"H2"}]^{(-1)} * (\text{Py}[\text{"CO"}] * \text{Py}[\text{"H2O"}] - (\text{Py}[\text{"H2"}] * \text{Py}[\text{"CO2"}]) / \text{Keq}[2])$
	Eqn21	●	$\text{RateRxn}[3] * \text{den}^2 * 3600 = k[3] * \text{Py}[\text{"H2"}]^{(-3.5)} * (\text{Py}[\text{"CH4"}] * \text{Py}[\text{"H2O"}]^2 - (\text{Py}[\text{"H2"}]^4 * \text{Py}[\text{"CO2"}]) / \text{Keq}[3])$

For the reverse of the water-gas shift and the methanation, the continuity equations are similar to those for steam reforming:

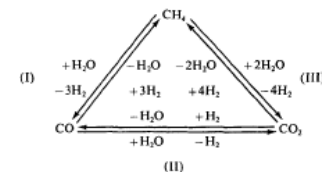
$$\frac{dx_{\text{CO}_2}}{d(W/F_{\text{CO}_2})} = r_{\text{CO}_2}$$

$$\frac{dx_{\text{CH}_4}}{d(W/F_{\text{CO}_2})} = r_{\text{CH}_4}$$

with boundary conditions at

$$W/F_{\text{CO}_2} = 0, \quad x_{\text{CO}_2} = x_{\text{CH}_4} = 0 \quad (2)$$

The reaction scheme leading to the retained set of rate equations and generated out of the detailed scheme of Figure 8, is shown in Table 3. This scheme is the detailed mechanistic expression of the following global triangular scheme (reactions I, II and III of Table 2):



The corresponding rate equations are:  
For reaction I of Table 3:

$$r_1 = \frac{k_1}{p_{\text{H}_2}^{1.5}} \left( p_{\text{CH}_4} p_{\text{H}_2\text{O}} - \frac{p_{\text{H}_2}^3 p_{\text{CO}}}{K_1} \right) / (\text{DEN})^2$$

For reaction II:

$$r_2 = \frac{k_2}{p_{\text{H}_2}} \left( p_{\text{CO}} p_{\text{H}_2\text{O}} - \frac{p_{\text{H}_2} p_{\text{CO}_2}}{K_2} \right) / (\text{DEN})^2 \quad (3)$$

For reaction III:

$$r_3 = \frac{k_3}{p_{\text{H}_2}^{3.5}} \left( p_{\text{CH}_4} p_{\text{H}_2\text{O}}^2 - \frac{p_{\text{H}_2}^4 p_{\text{CO}_2}}{K_3} \right) / (\text{DEN})^2$$

$$\text{DEN} = 1 + K_{\text{CO}} p_{\text{CO}} + K_{\text{H}_2} p_{\text{H}_2} + K_{\text{CH}_4} p_{\text{CH}_4} + K_{\text{H}_2\text{O}} p_{\text{H}_2\text{O}} / p_{\text{H}_2}$$

Reaction rates for the formation of CO and CO<sub>2</sub> and for the disappearance of methane in steam reforming are obtained from:

$$r_{\text{CO}} = r_1 - r_2$$

$$r_{\text{CO}_2} = r_2 + r_3$$

$$r_{\text{CH}_4} = r_1 + r_3 \quad (4)$$

Two of these rate equations are independent. These are the rate equations which were substituted into Eq. 1 for the data treatment of the steam reforming experiments.

Reaction rates for the disappearance of CO<sub>2</sub> and for the for-

**Table 3. Reaction Scheme and Corresponding Steps in Figure 8**

H <sub>2</sub> O	+ L	→ O-L	+ H <sub>2</sub>	(1)
CH <sub>4</sub>	+ L	→ CH <sub>3</sub> -L		(2)
CH <sub>3</sub> -L	+ L	→ CH <sub>2</sub> -L	+ H-L	(3)
CH <sub>2</sub> -L	+ L	→ CH-L	+ H-L	(4)
CH-L	+ O-L	→ CH <sub>2</sub> O-L	+ L	(21)
CH <sub>2</sub> O-L	+ L	→ CHO-L	+ H-L	(22)
CHO-L	+ L	→ CO-L	+ H-L	(23) r.d.s.; r <sub>1</sub>
CO-L	+ O-L	→ CO <sub>2</sub> -L	+ L	(8) r.d.s.; r <sub>2</sub>
CO-L	+ O-L	→ CO <sub>2</sub> -L	+ H-L	(25) r.d.s.; r <sub>3</sub>
CO-L		→ CO	+ L	(7)
CO <sub>2</sub> -L		→ CO <sub>2</sub>	+ L	(10)
2H <sub>2</sub> -L		→ H <sub>2</sub>	+ L	(1-bis)
H <sub>2</sub> -L		→ H <sub>2</sub>	+ L	(1-bis)

mation of CO and CH<sub>4</sub> in the reverse of the water-gas shift and methanation (CO<sub>2</sub> and H<sub>2</sub> as feed) are obtained from:

$$r_{\text{CO}} = r_1 - r_2$$

$$r_{\text{CO}_2} = -(r_2 + r_3)$$

$$r_{\text{CH}_4} = -(r_1 + r_3) \quad (5)$$

These are the rates which were substituted into Eq. 2.

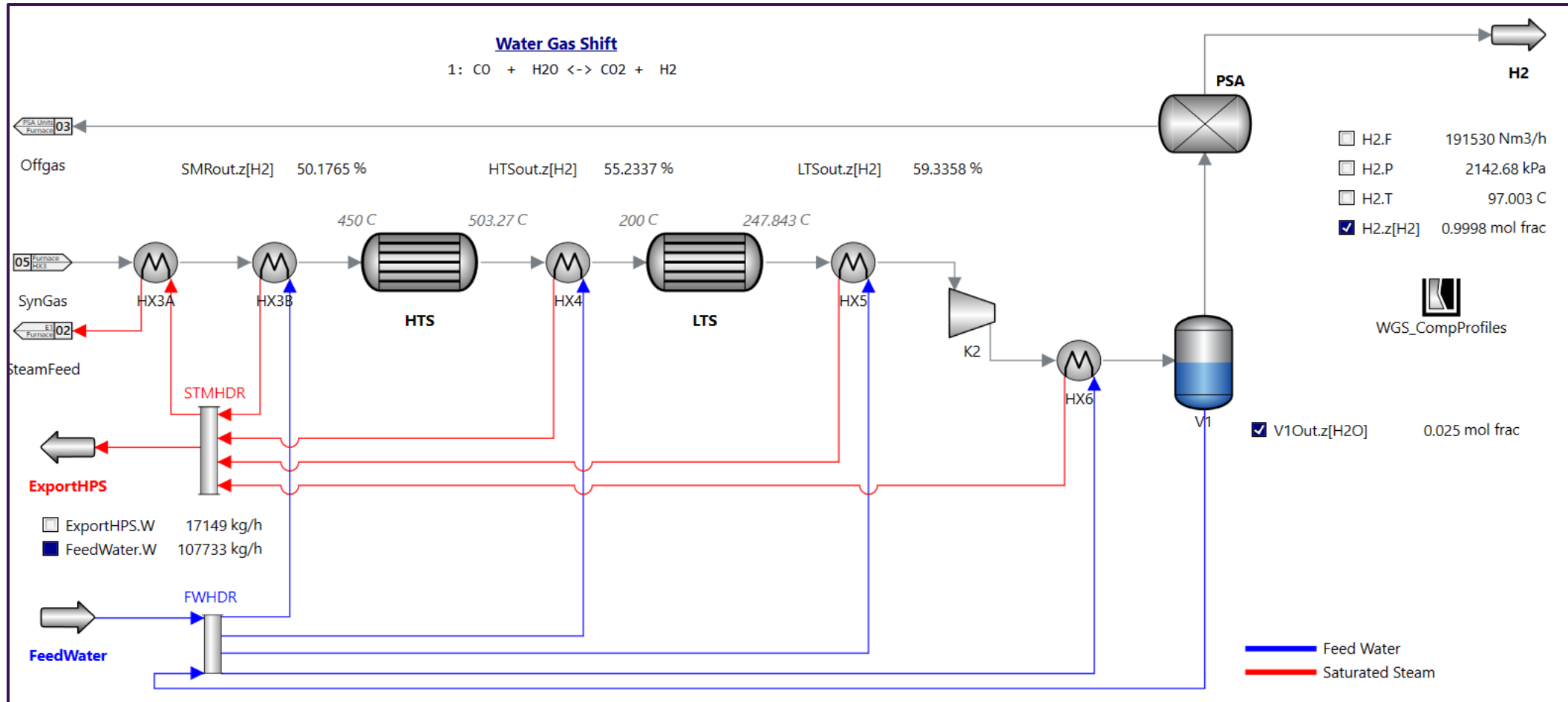
The adequacy of the fit of each of the 21 sets of rate equations was tested by means of the *F* value, the significance of the parameters by means of the *t* value and 95% confidence interval of the parameter estimates. The *F* value is calculated by dividing the mean squares due to regression (the sum of squares of the predicted responses divided by the number of parameters) by the mean residual squares (the sum of residual squares divided by the degree of freedom of residuals, which is the number of experiments minus the number of parameters). The *t* value of a parameter estimate is the ratio of the parameter estimate minus zero and the standard deviation of that parameter. If a parameter is found to have a very small *t* value or a large confidence interval including zero, it is considered to have no significant contribution to the rate equations. Consequently, it may be deleted from the latter.

## Results

Five of the 21 sets of rate equations generated out of the reaction schemes of Figures 7 and 8 were rejected after the model discrimination and parameter estimation based on the experimental results of steam reforming. This procedure was insufficient to discriminate further, since the *t* values of some of the parameters were too small, possibly because of a too narrow investigated temperature range. The model discrimination and parameter estimation including the reverse of the water-gas shift and methanation experiments allowed 15 of the remaining 16 sets of rate equations to be rejected.

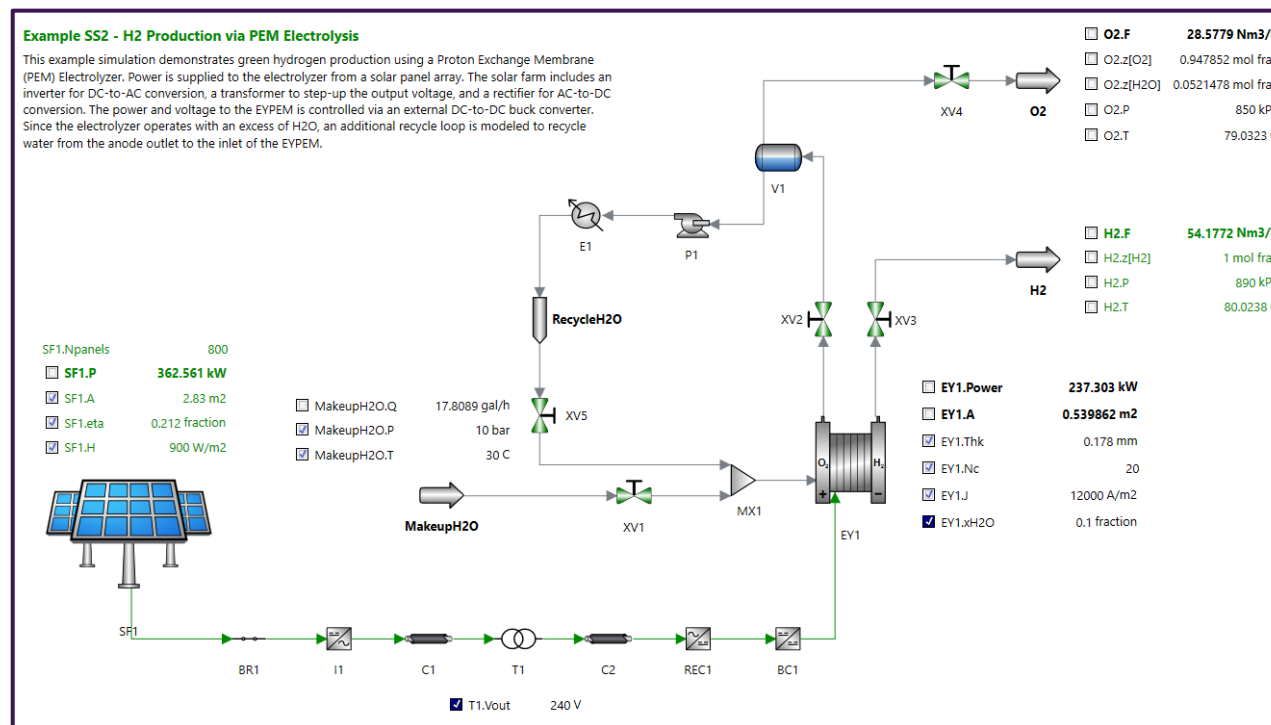
Since the partial pressures of CH<sub>4</sub> and H<sub>2</sub>O were low in the experiments on the reverse of water-gas shift and methanation, the adsorption coefficients *K*<sub>CH<sub>4</sub></sub> and *K*<sub>H<sub>2</sub>O</sub> could not be estimated significantly from these experiments. In the steam reforming experiments, the water-gas shift is very close to equilibrium so that *k*<sub>2</sub> cannot be estimated significantly at such conditions. The *k*<sub>3</sub> values were determined from the reverse water-gas shift and methanation data. Besides, for steam reforming conditions, the

J. Xu, G.F. Froment, Methane Steam Reforming, Methanation and Water-Gas Shift: I. Intrinsic Kinetics, AIChE J. 35 (1989) 88–96.



# Green Hydrogen – Electrolysis in AVEVA Process Simulation

- See Undocumented Example SS2 – H2 Production via PEM Electrolysis



# Electrolysis Modeling

## Electrolyzer Characteristics

- AVEVA Process Simulation allows you to edit key characteristics of the PEM Electrolyzer model and see the impact on overall hydrogen production:
  - Number of cells in series, **Nc**
  - Current density on electrolyzer stack, **J** (typically ~12 kA/m<sup>2</sup>)
- The EYPEM model includes an optional electrical connection
  - Electrolyzers require DC inputs so AC voltage must be first converted with a **Rectifier**
  - DC voltage is then stepped down with a Buck **Converter**. Choose between an Internal or External converter.

EY1 (Renewables.EYPEM)		
Configuration		
<input checked="" type="checkbox"/>	Converter	External
<input checked="" type="checkbox"/>	ModeCheck	Process
<input checked="" type="checkbox"/>	VohmType	Renewables.Vohm
<input checked="" type="checkbox"/>	VocType	Renewables.Voc
<input checked="" type="checkbox"/>	VactType	Renewables.Vact
Electrolyzer Data		
<input checked="" type="checkbox"/>	Thk	0.178 mm
<input type="checkbox"/>	A	0.539862 m2
<input checked="" type="checkbox"/>	Nc	20
Operation		
<input type="checkbox"/>	Pano	950 kPa
<input type="checkbox"/>	Pcat	940 kPa
<input checked="" type="checkbox"/>	DP	10 kPa
<input checked="" type="checkbox"/>	T	80 C
<input checked="" type="checkbox"/>	J	12000 A/m2
<input type="checkbox"/>	V	36.6302 V
<input type="checkbox"/>	I	6478.34 A
<input type="checkbox"/>	Power	237.303 kW
<input checked="" type="checkbox"/>	xH2O	0.1 fraction
Products		
Voltage		
Heat		
Ohmic Resistance		
No Group		

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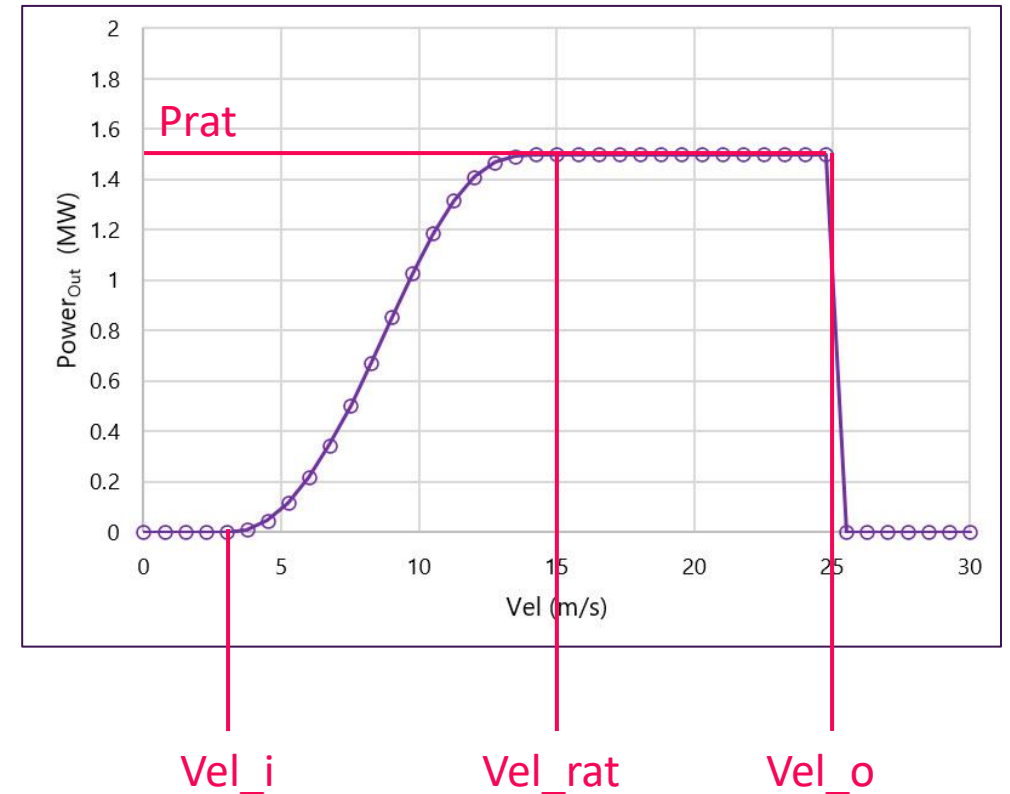
# Renewable Energy Models in AVEVA Process Simulation



# Wind Farm Modeling

## Power Curves

- AVEVA Process Simulation uses turbine power curves for calculating output power and the power coefficient
- **DefWFPower** is the default scaled power curve and represents a typical turbine. You should specify:
  - $Prat$  – Rated power output of the turbine
  - $Vel\_i$  – Cut-in velocity (typically 3-4 m/s)
  - $Vel\_rat$  – Wind velocity at rated power (typically 11-17 m/s)
  - $Vel\_o$  – Cut-out velocity (typically ~25 m/s)
- You can also select a custom power curve for your turbines

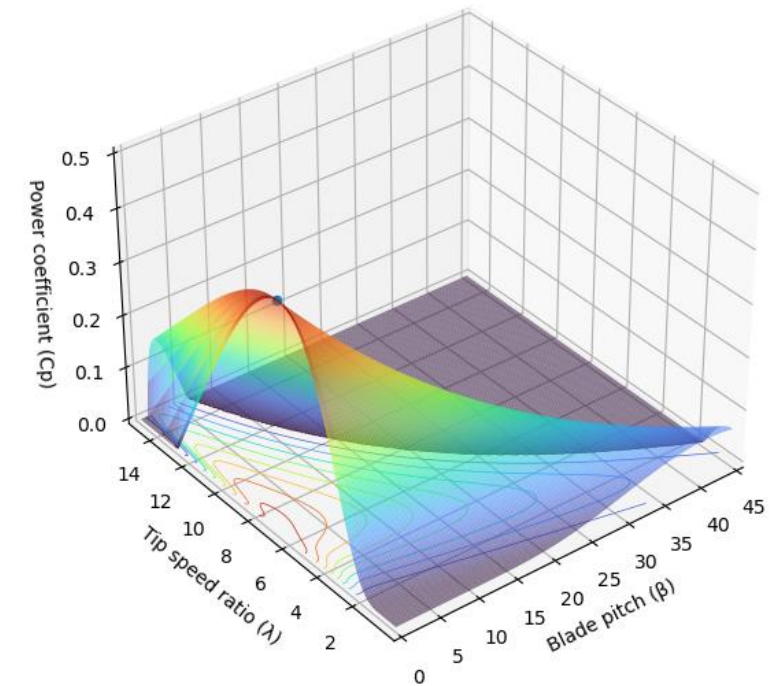


# Wind Farm Modeling



## What is the Power Coefficient ( $C_p$ )?

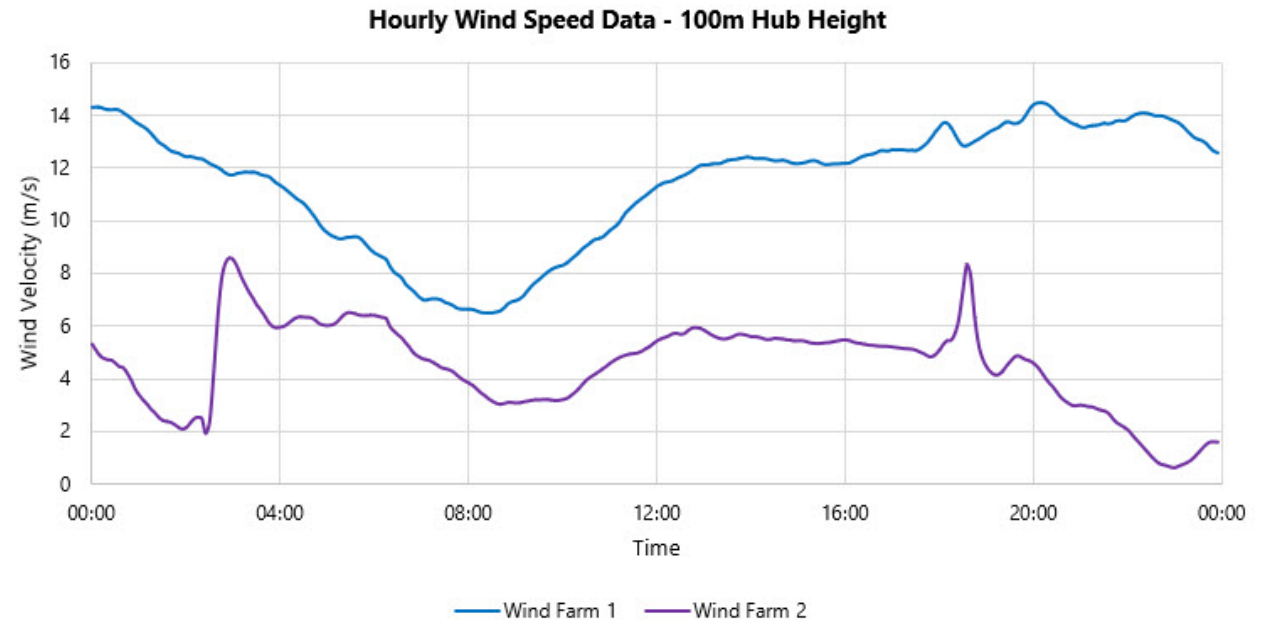
- Indicates how much of the total wind energy is captured by the turbine after aerodynamic, mechanical, and electrical losses
- It has an upper limit of 59.3% for an ideal turbine (Betz's Law)
- Broadly,  $C_p$  is a function of:
  - Blade tip speed ratio ( $\lambda$ ) – wind speed vs. rotational speed of turbine
  - Blade pitch angle ( $\beta$ )
- Turbine controllers attempt to maintain  $C_{p_{\max}}$  by adjusting  $\lambda$  and  $\beta$
- AVEVA Process Simulation calculates  $C_p$  directly from the power output



# Wind Farm Modeling

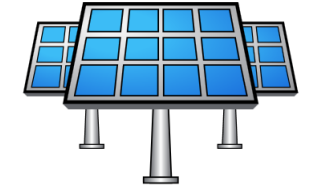
## Specifying Wind Velocity

- In Process mode, specify the average velocity, **Vel**, to calculate output power
- In Dynamics mode, provide a time vs. velocity trend and use the curve tracing features to see how power output changes throughout the day
- Where to find wind resource data?
  - National Renewable Energy Laboratory (NREL) [Wind Integration National Dataset](#) (WIND)





# Solar Farm Modeling

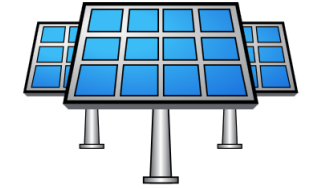


## Panel Characteristics

- Solar panel output power is a function of:
  - Solar irradiance (**H**)
  - Panel area (**A**)
  - Module efficiency (**eta**) – fraction of total energy captured by the panel at standard test conditions ( $H = 1000\text{W/m}^2$ ,  $T = 25^\circ\text{C}$ ). This is provided by the manufacturer and typically ranges from 10 – 25%.
  - Cell temperature (**T<sub>c</sub>**) and temperature coefficient of power (**alpha**)
  - Performance Ratio (**PR**) – accounts for total losses beyond those reported by manufacturer

SF1 (Renewables.SolarFarm)		
Configuration		
	Npanels	8000
	SolarTrend	Models.SolarTrend
	<input checked="" type="checkbox"/> A	2.83 m2
	<input checked="" type="checkbox"/> eta	0.212 fraction
	<input checked="" type="checkbox"/> alpha	-0.47 %/C
Operation		
	<input checked="" type="checkbox"/> H	900 W/m2
	<input type="checkbox"/> PR	0.87696 fraction
	<input checked="" type="checkbox"/> Tc	27.85 C
	<input type="checkbox"/> P	3.7348 MW
	<input type="checkbox"/> Ps	466.85 W
> Losses		
> Electrical		
> No Group		

# Solar Farm Modeling



## Performance Ratio

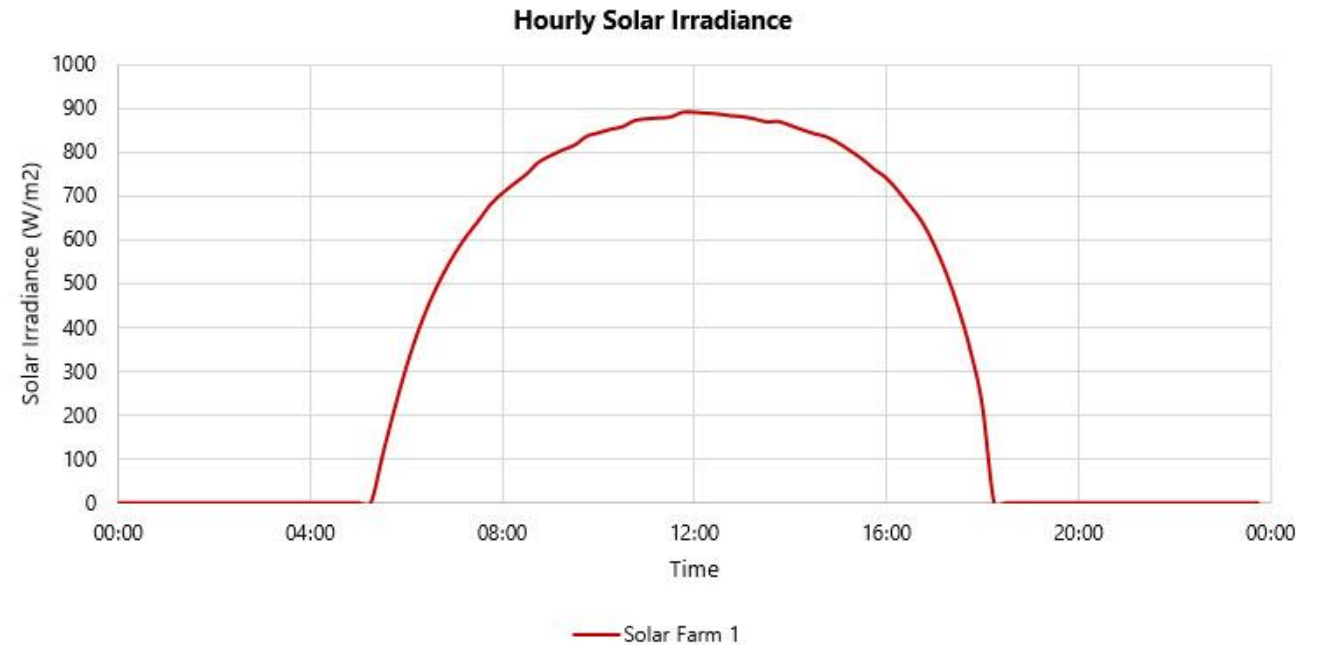
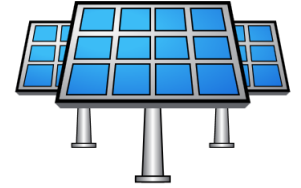
- Performance Ratio (PR) accounts for losses not measured by manufacturer:
  - Soiling – dust and dirt on panels
  - Shade
  - Snow
  - Mismatched voltage and current characteristics between panels
  - Panel age
  - Light-induced degradation
- AVEVA Process Simulation uses default values recommended by the National Renewable Energy Laboratory (NREL)

SF1 (Renewables.SolarFarm)		
Configuration		
Operation		
Losses		
<input checked="" type="checkbox"/>	Lsoil	0.02 fraction
<input checked="" type="checkbox"/>	Lshade	0.03 fraction
<input checked="" type="checkbox"/>	Lsnow	0 fraction
<input checked="" type="checkbox"/>	Lmis	0.02 fraction
<input checked="" type="checkbox"/>	Lwire	0.02 fraction
<input checked="" type="checkbox"/>	Lconn	0.005 fraction
<input checked="" type="checkbox"/>	Ldeg	0.015 fraction
<input checked="" type="checkbox"/>	Lrate	0.01 fraction
<input checked="" type="checkbox"/>	Lage	0 fraction
<input checked="" type="checkbox"/>	Lavail	0.03 fraction
<input type="checkbox"/>	Ltotal	0.140757 fraction
Electrical		
No Group		

# Solar Farm Modeling

## Specifying Solar Irradiance

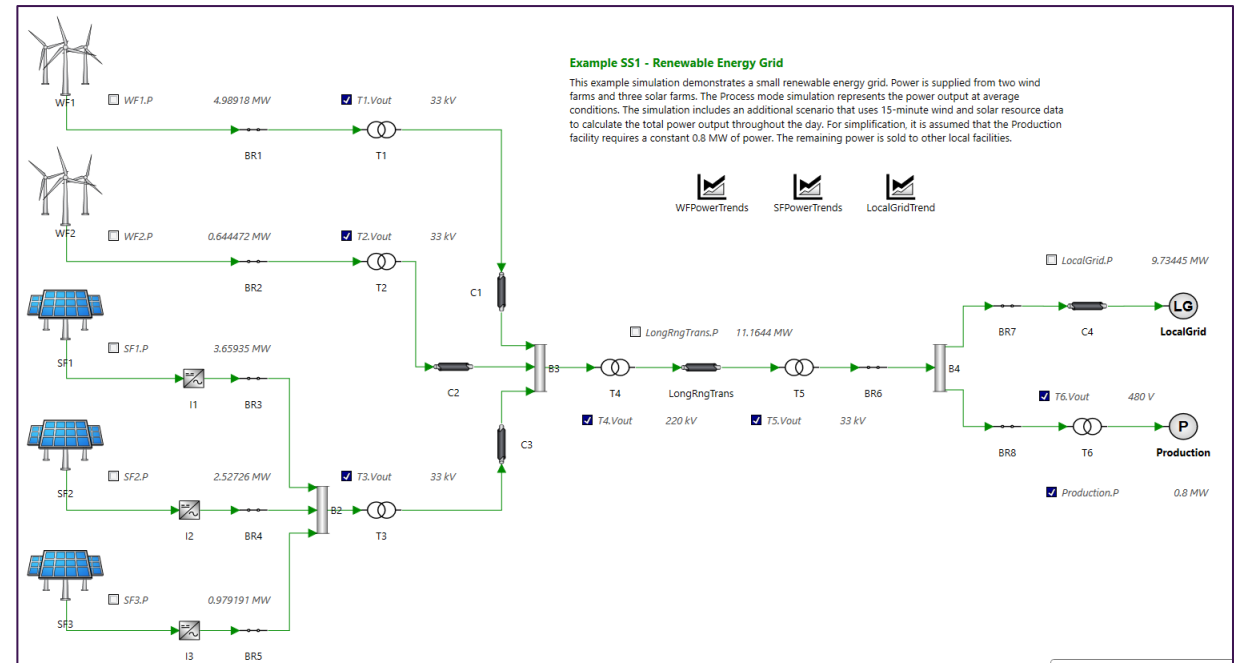
- In Process mode, specify the average solar irradiance, **H**, to calculate output power
- In Dynamics mode, provide a time vs. solar resource trend and use the curve tracing features to see how power output changes throughout the day
- Where to find solar resource data?
  - National Renewable Energy Laboratory (NREL) [National Solar Radiation Database](#) (NSRDB) – data available for the United States, South Asia, and Mexico/Central America



# Renewable Grid Modeling

## Connecting Renewable Energy Sources to Plant Equipment

- AVEVA Process Simulation includes a variety of simplified models to simulate a full renewable energy grid:
  - Transformer (AC → AC)
  - Converter (DC → DC)
  - Inverter (DC → AC)
  - Rectifier (AC → DC)
  - Transmission Cable
  - Busbar
  - Breaker
  - Generator



See Example SS1 – Renewable Energy Grid

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# Takeaways – Why AVEVA Process Simulation?





# Optimize Existing Plants and Processes

## Greenhouse Gas Emissions

- Use AVEVA Process Simulation to add greenhouse gas emission calculations to your simulations
- Almost every process has emissions that can be reduced
- GHG models are drag-and-drop and require almost no additional engineering effort
- Access the full range of features in AVEVA Process Simulation for optimization and dynamic studies



# Quicky Adapt to Emerging Technologies

## Hydrogen Production and Renewable Energy

- AVEVA Process Simulation can be used to model the entire hydrogen value chain
- There are opportunities for improving Grey Hydrogen processes with advanced reaction kinetics and GHG models
- Pivot to new technologies with the Renewables library (renewable energy and water electrolysis)
- The open model writing framework allows you to quickly adapt to changing technologies as they become available commercially



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